

# Grain Size Distribution Documentation of Calculations

The calculations used in the program are fairly simple and for the most part follow ASTM D422. The following sections present the equations used.

## 1 Moisture Content

Moisture content is calculated with the following formula:

$$MC = 100\% * \frac{W_{wt} - W_{dt}}{W_{dt} - W_t} \quad (1.1)$$

**Where:**

MC = the moisture content

$W_{wt}$  = the weight of the moisture specimen with tare

$W_{dt}$  = the weight of the dried specimen with tare

$W_t$  = the weight of the container

## 2 Sieve Test Calculations

### 2.1 Wash Test

$$PF_{200} = \frac{W_{ts} - W_{wash}}{W_{ts}} * 100\% \quad (1.2)$$

**Where:**

$PF_{200}$  = the percent of material finer than the #200 sieve

$W_{ts}$  = the total sample weight

$W_{wash}$  = the after-wash weight

The program charts  $PF_{200}$  as the #200 percentage if either no further sieve test data are entered (i.e., only a #200 wash test is performed), or the sieve test does not include a #200 sieve.

## 2.2 Cumulative Weight Retained Method

$$PF = \left(1 - \frac{W_c - W_{ct}}{W_{ts}}\right) * 100\% \quad (1.3)$$

**Where:**

PF = the percent finer  
 $W_c$  = the cumulative weight retained  
 $W_{ct}$  = the tare weight of the cumulative pan  
 $W_{ts}$  = the total sample weight

**An example calculation:**

Cumulative weight retained = **1915.2** grams  
 Cumulative pan tare = **382.5** grams  
 Sample weight = **1671.4** grams

$$PF = \left(1 - \frac{1915.2 - 382.5}{1671.4}\right) * 100\% = 8.3\%$$

## 2.3 Per-Sieve Weight Retained Method

$$PF = 1 - \frac{(W_{st} - W_t) + W_{ls}}{W_{ts}} * 100\% \quad (1.4)$$

**Where:**

$W_{st}$  = the weight of a sieve and its retained material  
 $W_t$  = the weight of the sieve  
 $W_{ls}$  = the total amount of material retained on all larger sieves  
 $W_{ts}$  = the weight of the total sample

**An example calculation:**

To calculate the percent finer for the third largest sieve in a sieve nest, we need:

Total sample weight = **11.94** grams  
 Weight retained + tare for the third largest sieve = **9.66** grams  
 Tare weight for the third largest sieve = **4.19** grams  
 Material retained on the larger sieves: **0.00** grams on the largest + **0.54** grams on the second largest.

$$PF = 1 - \frac{(9.66 - 4.19) + 0.54}{11.94} * 100\% = 49.7\%$$

## 2.4 Sample Splits

If the sample is split, the subsequent percent finer values are found as follows:

$$PF_{tot} = \frac{CBT - WR}{DWT} \quad (1.5)$$

**Where:**

PF<sub>tot</sub> = the overall percent finer

WR = the weight retained of the split sample

DWT, the post-split sample dry weight, is calculated as follows:

$$DWT = \frac{SGDW}{PF_{ss} - PFW} \quad (1.6)$$

**Where:**

SGDW = the split gradation dry sample weight

PF<sub>ss</sub> = the overall percent finer than the split sieve

PFW = the percent washed out from the #200 wash test (or 0 if a wash test was not performed)

CBT, the biased total weight, is calculated as follows:

$$CBT = SGDW + PFW * DWT \quad (1.7)$$

**An example calculation:**

PF<sub>ss</sub> = **72.3** %

SGDW = **1871.30** grams

PFW = **0.00** %

WR = **422.00** grams

$$DWT = \frac{1871.30}{72.30 - 0.00} = 25.90$$

$$CBT = 1871.30 + (0.00 * 25.9) = 1871.30$$

$$PF = \frac{1871.30 - 442.00}{25.90} = 55.2\%$$

### 3 Hydrometer Test Calculations

#### 3.1 Particle Size

$$PS = \sqrt{\frac{30 * v * l}{980 * (GS - GW) * ET}} \quad (1.8)$$

**Where:**

Ps = the particle size in mm.

v = the fluid viscosity in centipoises

L = the effective depth in cm.

GS = the specific gravity of the soil particles

GW = the specific gravity of water, corrected for temperature

Et = the elapsed time in minutes

For 152H hydrometers, L, the effective depth, is calculated as follows:

$$L = 16.295 - 0.164 * Rm \quad (1.9)$$

**Where:**

Rm = the hydrometer reading corrected by subtracting the absolute value of the meniscus correction

This equation is equivalent to the 152H equation given by ASTM D422 et al.:

$$L = L_1 + 0.5 * (L_2 - \frac{V_b}{A}) \quad (1.10)$$

**Where:**

$$L_1 = \frac{50 - Rm}{50 - 0} (10.5 - 2.3) + 2.3 \quad (1.11)$$

$L_2 = 14.0\text{cm.}$

$V_b = 67.0\text{cm.}^3$

$A = 27.8\text{cm.}^2$

Substituting, D422's effective depth equation becomes:

$$L = [\frac{50}{50} * (10.5 - 2.3) - Rm/50 * (10.5 - 2.3) + 2.3] + [0.5 * 14 - \frac{0.5 * 67.0}{27.8}] \quad (1.12)$$

which, after simplifying, is identical to our equation.

For 151H hydrometers L is calculated with this equation (with D422 derivation similar to the prior 152H equation):

$$L = 16.295 - 0.2645 * Rm \quad (1.13)$$

⇒ Note that the effective depth equation can be changed by the user on a per-test basis.

$\nu$ , the fluid viscosity, is calculated as:

$$\nu = C1 + T * (C2 + T * (C3 + T * (C4 + T * C5))) \quad (1.14)$$

**Where:**

T = the fluid temperature, in degrees Celsius

C1 = 0.01732483379693

C2 = -5.041574656095E-04

C3 = 8.387438669317E-06

C4 = -7.401129271698E-08

C5 = 2.625994080072E-10

GW, the specific gravity of water, is calculated as:

$$GW = C1 + T * (C2 + T * (C3 + T * C4)) \quad (1.15)$$

**Where:**

T = the fluid temperature, in degrees Celsius

C1 = 0.99991003252

C2 = 0.00005201921

C3 = -0.00000751229

C4 = 0.00000003605183

**An example calculation:**

ET = 8 minutes

Temp = 23.5 Celsius

R = 34

Cm = 1

GS = 2.7

Rm = 35 (= R + Cm)

GW = 0.997452 (calculation not shown)

v = 0.00925 (calculation not shown)

L = 10.56 (calculation not shown)

$$PS = \sqrt{\frac{30 * 0.00925 * 10.56}{980 * (2.7 - 0.9975) * 8}} = 0.0148 \text{ mm.}$$

### 3.2 Percent Finer

For 152H hydrometers, the percent finer than a given opening size is calculated as:

$$PF = \frac{Rc * a}{WB} * 100\% \quad (1.16)$$

**Where:**

- PF = the percent finer
- Rc = the corrected hydrometer reading
- a = the specific gravity of solids correction factor
- WB = the biased hydrometer sample weight

For 151H hydrometers, the calculation is:

$$PF = \frac{100 * GS}{WB * (GS - 1)} * Rc \quad (1.17)$$

**Where:**

- PF = the percent finer
- Rc = the corrected hydrometer reading
- WB = the biased hydrometer sample weight
- GS = the soil specific gravity

When using automatic temperature correction, the corrected hydrometer reading (Rc) is calculated as follows:

$$Rc = R + Ct + Cc \quad (1.18)$$

**Where:**

- R = the actual hydrometer reading (in thousandths for 151H)
- Cc = the composite correction at 20 degrees Celsius, as entered by the user
- Ct = the composite correction

For 152H hydrometers, Ct, the composite correction, is calculated as follows:

$$Ct = -12.35952257 + T * (1.51062059 + T * (-0.06923056 + T * 0.00122483)) \quad (1.19)$$

**Where:**

- T = the fluid temperature, in degrees Celsius

For 151H hydrometers, Ct is calculated as:

$$Ct = -7.6338851 + T * (0.93361976 + T * (-0.04284159 + T * 0.000758977)) \quad (1.20)$$

**Where:**

- T = the fluid temperature, in degrees Celsius

When using the multi-point (linear) temperature correction, the corrected hydrometer reading is calculated as follows:

$$R_c = R + Ct \quad (1.21)$$

**Where:**

R = the actual hydrometer reading (in thousandths for 151H)

Ct = the temperature correction, as interpolated from a linear regression line constructed from the pairs of temperature and reading values entered by the user into the hydrometer correction grid.

- For test temperatures less than the lowest temperature entered into the correction grid, the program will use the correction value corresponding to the lowest correction temperature entered; likewise, for test temperatures higher than the highest temperature entered into the correction grid, the program will use the correction value corresponding to the highest correction temperature entered.

The specific gravity correction factor is:

$$a = \frac{0.6226415 * GS}{GS - 1} \quad (1.22)$$

**Where:**

GS = the specific gravity of the solids

The biased sample weight is calculated as:

$$WB = \frac{Whs * 10000}{Pss * (100 + Mh)} \quad (1.23)$$

**Where:**

WB = the biased sample weight, in grams

Whs = the air dry hydrometer sample weight

PSS = the percent passing the separation sieve

Mh = the hygroscopic moisture content per ASTM D422 § 8

**An example calculation using a 152H hydrometer:**

ET = **8** minutes

Temp. = **23.5** degrees Celsius

R = **34**

GS = **2.7**

Mh = **3.5%**

Linear correction pairs: (-6.0 at 20°), (-5.6 at 22°), (-4.7 at 25°)

By interpolation, Cc at 23.5° = -5.15

$$Rc = 34 + (-5.15) = 28.9$$

$$a = \frac{0.6226415 * 2.7}{2.7 - 1} = 0.989$$

$$WB = \frac{51.7 * 10000}{100 * (100 + 3.5)} = 50.0 \text{ grams}$$

$$PF = \frac{28.9 * 0.989}{50.0} = 57.0\%$$

**An additional calculation, using a 151H hydrometer:**

ET = **15** minutes

Temp = **22** Celsius

R = **21.5**

GS = **2.65**

WB = **63.5** grams

Cc at 22 degrees Celsius = **-2.2**

$$Rc = 21.5 + (-2.2) = 19.3$$

$$PF = \frac{100 * 2.65}{63.5 * 1.65} * 19.3 = 48.8\%$$

### 3.3 Calculation of Fractional Components

The fractional components and percentage diameters ( $D_{85}$ ,  $D_{60}$ ,  $D_{50}$ , etc.) are computed by creating a cubic spline model of the particle size distribution curve then solving the model for the curve values at various percentages.

The classification coefficients  $C_c$  and  $C_u$  are calculated as follows:

$$C_c = \frac{D_{30} * D_{30}}{D_{60} * D_{10}} \quad (1.24)$$

$$C_u = \frac{D_{60}}{D_{10}} \quad (1.25)$$

### 3.4 Tables of Constants

Table 1.1: Correction Factor for Specific Gravities Other than 2.65 when using Hydrometer 152H

SPECIFIC GRAVITY	CORR. FACTOR	SPECIFIC GRAVITY	CORR. FACTOR
2.50	1.038	2.68	0.994
2.51	1.036	2.69	0.992
2.52	1.033	2.70	0.989
2.53	1.030	2.71	0.987
2.54	1.028	2.72	0.985
2.55	1.025	2.73	0.983
2.56	1.022	2.74	0.981
2.57	1.020	2.75	0.979
2.58	1.017	2.76	0.977
2.59	1.015	2.77	0.975
2.60	1.012	2.78	0.973
2.61	1.010	2.79	0.971
2.62	1.008	2.80	0.969
2.63	1.005	2.81	0.967
2.64	1.003	2.82	0.965
2.65	1.001	2.83	0.963
2.66	0.998	2.84	0.962
2.67	0.996	2.85	0.960

Table 1.2: Automatic Temperature Correction Factor as a Function of Temperature

TEMP, DEG C.	SPECIFIC GRAVITY OF WATER	VISCOSITY OF WATER	TEMP. CORR. FACTOR FOR 152H	TEMP. CORR. FACTOR FOR 151H
15.0	0.99912	0.01141	-1.14	-0.71
15.5	0.99050	0.01126	-1.02	-0.63
16.0	0.99897	0.01111	-0.90	-0.55
16.5	0.99889	0.01097	-0.78	-0.48
17.0	0.99880	0.01083	-0.67	-0.41
17.5	0.99871	0.01069	-0.56	-0.35
18.0	0.99862	0.01056	-0.46	-0.28
18.5	0.99853	0.01043	-0.35	-0.22
19.0	0.99843	0.01030	-0.25	-0.16
19.5	0.99834	0.01017	-0.15	-0.09
20.0	0.99823	0.01005	-0.04	-0.03
20.5	0.99813	0.00993	0.07	0.04
21.0	0.99802	0.00981	0.18	0.11
21.5	0.99791	0.00969	0.29	0.18
22.0	0.99780	0.00958	0.41	0.25
22.5	0.99769	0.00947	0.53	0.33
23.0	0.99757	0.00936	0.66	0.41
23.5	0.99745	0.00925	0.80	0.50
24.0	0.99733	0.00914	0.95	0.59
24.5	0.99721	0.00904	1.11	0.69
25.0	0.99708	0.00894	1.27	0.79
25.5	0.99695	0.00884	1.45	0.90
26.0	0.99682	0.00874	1.64	1.02
26.5	0.99668	0.00864	1.85	1.15
27.0	0.99655	0.00855	2.07	1.28
27.5	0.99641	0.00846	2.30	1.43
28.0	0.99627	0.00836	2.55	1.58
28.5	0.99613	0.00827	2.81	1.75
29.0	0.99598	0.00818	3.10	1.92
29.5	0.99583	0.00809	3.40	2.11
30.0	0.99568	0.00801	3.72	2.31

Table 1.3: Effective Depth for 152H and 151H Hydrometers

Rm	EFFEC-TIVE DEPTH	Rm	EFFEC-TIVE DEPTH	Rm	EFFEC-TIVE DEPTH	Rm	EFFEC-TIVE DEPTH
0	16.3	26	12.0	0	16.3	20	11.0
1	16.1	27	11.9	1	16.0	21	10.7
2	16.0	28	11.7	2	15.8	22	10.5
3	15.8	29	11.5	3	15.5	23	10.2
4	15.6	30	11.4	4	15.2	24	9.9
5	15.5	31	11.2	5	15.0	25	9.7
6	15.3	32	11.0	6	14.7	26	9.4
7	15.1	33	10.9	7	14.4	27	9.2
8	15.0	34	10.7	8	14.2	28	8.9
9	14.8	35	10.6	9	13.9	29	8.6
10	14.7	36	10.4	10	13.7	30	8.4
11	14.5	37	10.2	11	13.4	31	8.1
12	14.3	38	10.1	12	13.1	32	7.8
13	14.2	39	9.9	13	12.9	33	7.6
14	14.0	40	9.7	14	12.6	34	7.3
15	13.8	41	9.6	15	12.3	35	7.0
16	13.7	42	9.4	16	12.1	36	6.8
17	13.5	43	9.2	17	11.8	37	6.5
18	13.3	44	9.1	18	11.5	38	6.2
19	13.2	45	8.9	19	11.3		
20	13.0	46	8.8				
21	12.9	47	8.6				
22	12.7	48	8.4				
23	12.5	49	8.3				
24	12.4	50	8.1				
25	12.2						